INTRODUCTION

Nowadays, atmospheric pressure low temperature plasmas are applied in many industrial processes. They are: treatment of flue gases emitted by industrial processes of combustion, painting and varnishing, wastes utilization, deodorization, disinfection and sterilization [Stryczewska et al. 2013], material processing and new material manufacturing for application in microelectronics and nanotechnologies. Non-thermal and non-equilibrium plasma-based methods allow treatment of organic materials, like rubber, fabrics, biomaterials [Kovaľová 2013] and they are ecologically justified alternative for chemical ones [Addou et al 2005, Brisset & Pawłat 2016].

In Poland, the plasma processes, although investigated in research laboratories, are applied in industry at much smaller scale than in industrialized countries of Europe and the rest of the world [Sawicki & Krouchinin 2000]. Polish power industry is based on fossil fuels combustion that emits pollution in form of sulfur and nitrogen oxides, soot and ashes, which have to be disposed of. Plasma technologies can be a reasonable alternative for chemical, gypsum-based wet methods, environmentally noxious, still applied in power industrial practice.

Investigations in the field of industrial application of plasma chemical methods, conducted in many research centers and universities in Poland and abroad, are now concentrated on obtaining controllable plasma parameters and chemical reactions in a large volume of treated gases [Pawłat et al. 2011]. Repeatability of the plasma-chemical process depends on stability of plasma parameters, which influence the proper chemical reaction path. The main parameters are the chemical composition of the plasma gas, its pressure, flow rate, geometry of plasma reactor and electrical parameters of power system, i.e. value and form of supply voltage, power, and frequency [Mazurek 2011].

Arc discharge can be a source of non-thermal and non-equilibrium plasma at certain conditions of power supply system, geometry of reactor electrodes and gas flow rate [Heeren et al. 2005]. The gliding arc discharge plasma is an example of this kind of low temperature plasma that can be generated in multi-electrode reactors at atmospheric pressure.

Gliding arc reactor considerably differs from other non-thermal plasma sources [Czernichowski 1994, Lesueur et al. 1990]. The resistance of inter-electrode gap depends on the kind of gas, its flow rate, degree of ionization and it also changes its value in wide range during the single opera-
Based on the estimated temperatures $T_e$, $T_{\text{rot}}$ and $T_{\text{vib}}$ we can conclude equilibrium or non-equilibrium character of generated plasma.

The main problem in the optical plasma diagnostic is difficult manual calculation [10, 11] of particle temperatures from the plasma emission spectrum. In order to confirm to non-equilibrium of generated plasma we only need to know electron temperature ($T_e$) and gas temperature ($T_{\text{rot}}$). The electron temperature can be easily estimated based on relative intensities of argon emission lines and gas temperature can be measured with a thermovision camera.

EXPERIMENTAL METHODS

Different diagnostic methods can be used to determine electrons and gas temperature. The electrons' temperature has been determined by optical spectroscopy and gas temperature – by thermovision camera. Optical diagnostic of the gliding arc discharge plasma can be a reliable source of information on concentrations and temperatures of plasma components in atmospheric gases [Diatczyk et al. 2006]. Non-equilibrium condition of plasma generated by gliding arc discharge, including changes of ionization type from thermal to non-thermal, together with low resolution of CCD spectrometers requires specific approach to its spectral diagnostic [10, 11].

The purpose of spectral diagnostic of plasma generated in gliding arc discharge reactor is to determine the plasma particles energy distribution.

RESULTS AND DISCUSSION

Experimental setup

We use the VIGO System V-20 ER005–10 thermovision camera (Fig. 1) with spatial resolution – $3.5 \times 10^{-3}$ rad and spectral range $3–5 \times 10^{-6}$ m. It measures averaged in time gas temperature (10 s for matrix; 0.1 s for single line). In experiment the focal length is: 1.20 m for horizontal position, 0.90 m for vertical position and 1.10 m for look down view.

For optical diagnostic we use a USB spectrometer based on CCD line, Solar TII SL40–2–3648 USB. The spectrometer can provide spectra in range $190 \times 10^{-9} – 1100 \times 10^{-9}$ m with optical resolution of about $1 \times 10^{-9}$ m. Plasma was generated in the chamber of gliding arc plasma reactor (Fig. 2) in argon, nitrogen and air, respectively.
We use different gas flow rates – ranging from 0.3 m$^3$/h to 3.5 m$^3$/h. The gas flow lesser than 0.5 m$^3$/h was used only for argon, in which discharge can be sustained at much lower voltage than in nitrogen and air. Gas temperature has been measured along two axes: horizontal and vertical (Fig. 3). Diagnostic conditions and reactor geometry are given in table 1.

**Thermovision diagnostic results**

Based on results of the thermovision diagnostic, temperature distribution in the discharge chamber of the plasma reactor for different argon flow rates has been studied (Fig. 4).

The temperature inside the chamber of plasma reactor decreases with the growth of the argon flow rate (Fig. 4). For argon flow rates lesser than 1.0 m$^3$/h the temperature changes are insignificant. Argon flow rate change in the range from 0.3 m$^3$/h to 1.0 m$^3$/h causes the temperature changes lesser than 10%. Increase the argon flow rate above 1.0 m$^3$/h results in significant fall of the temperature inside the reactor chamber.

Moreover, changes of the temperature distribution in the chamber of the plasma reactor for different gases and constant flow rate have been examined (Fig. 5).

Chemical composition of the processing gas together with gas flow rate growth causes the changes of temperature distribution in the gliding arc discharge chamber. In the case of nitrogen and air, the temperature inside the chamber of the plasma reactor is about 30% higher in comparison to argon as a processing gas.

**Table 1. Conditions of the temperature measurements**

<table>
<thead>
<tr>
<th>Discharge chamber geometry</th>
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<tbody>
<tr>
<td>chamber diameter</td>
<td>0.080 m</td>
</tr>
<tr>
<td>electrode length</td>
<td>0.141 m</td>
</tr>
<tr>
<td>electrode distance in the ignition area</td>
<td>(1 - 6)´10$^{-3}$ m</td>
</tr>
<tr>
<td>electrode distance in the extinction area</td>
<td>0.030 - 0.035 m</td>
</tr>
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**Gas parameters**

<table>
<thead>
<tr>
<th>Process gases</th>
<th>argon, air, nitrogen</th>
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<tbody>
<tr>
<td>Gas flow rates</td>
<td>0.3 - 3.5 m$^3$/h</td>
</tr>
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**Power supply system parameters**

<table>
<thead>
<tr>
<th>Inter-electrode voltage</th>
<th>400 - 1500 V</th>
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<tbody>
<tr>
<td>Electrode current</td>
<td>1.0 - 3.5 A</td>
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**Figure 3.** Vertical and horizontal lines for thermovision measurements.

**Figure 4.** The temperature distribution in the chamber of gliding arc plasma reactor for different argon flow rates.

**Figure 5.** The temperature distribution in the chamber of gliding arc plasma reactor for different gases and constant flow rate (1.5 m$^3$/h).
Spectroscopic diagnostic results

The electrons’ temperature ($T_e$), which corresponds to the electron population distribution, has been determined by spectroscopic method on the basis of Boltzmann plot by using the relative intensities of copper (Cu) emission lines: 465.1·10^{-9} m, 510.5·10^{-9} m, 515.3·10^{-9} m, 521.8·10^{-9} m, 578.2·10^{-9} m, respectively. Selection of these lines is conditioned as follows [10]:

- there is no overlapping of these lines with other spectral lines and bands,
- the energy differences between the upper excited levels of spectral transitions are high enough to reduce inaccuracy in temperature estimations.

Determination of the vibration temperature $T_{vib}$ (the temperature of vibration levels population distribution) was based on measuring relative intensities of nitrogen ($N_2$) spectral emission bands. This method assumed that vibration temperatures of the ground state and electronic excited states are very closed. The vibration temperature $T_{vib}$ can be also determined from the Boltzmann plot.

Generally, in non-equilibrium air plasmas, distribution of electronic population can be different from the Boltzmann plot [Raniszewski 2013]. Therefore, at first we must check the Boltzmann energy distribution law.

Spectroscopic measurements were performed for argon, air and nitrogen at flow rates from 0.5 m$^3$/h to 3.5 m$^3$/h. The spectra presented in the Figure 6 show that technological gases used in experiments contain impurities (Fig. 6). The plasma gas contains also contains coming from electrodes due to the spark erosion [Присяжневич et al. 2005]. Reactor electrodes applied in experiments made of acid-resistance steel consist quite large content of chrome and nickel, and also some manganese, titanium, molybdenum and copper.

CONCLUSIONS

Temperature distribution in the discharge chamber of plasma reactor with gliding arc is a very important factor from the point of view of plasma chemistry, and determines the technological application of this kind of plasma.

Gas temperature can be determined with the aid of thermovision technique, while electrons energy, usually several times greater than that of gas, from optical spectroscopy. Combination of these methods can be a suitable tool for estimation plasma non-equilibrium.

The optical on-line analysis of the plasma spectrum during the discharge together with current and voltage measurements can be used to control the dynamic characteristics of the gliding arc plasma reactor almost in real time. The spectroscopic characterization of the gliding arc discharge plasma can also be useful in explaining the mechanism of its transition from equilibrium to non-equilibrium state and to giving directions how to design power system in order to ensure the time of the non-equilibrium and non-thermal plasma state much longer than the equilibrium and thermal one.

The temperature in the chamber of plasma reactor declines along with the growth of the gas flow rate [14].

Argon used as the processing gas causes significantly lower temperature inside the chamber of the plasma reactor.

Electron temperature (about 8000 K) in the gliding arc discharge plasma obtained by opti-
cal spectroscopy diagnostic referenced to the gas temperature (about 600 K) from thermovision camera indicates that the generated plasma is non-thermal and non-equilibrium.

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**REFERENCES**