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Characteristics and potential use of residual waste from bauxite ore processing industry in West Kalimantan, Indonesia

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ABSTRACT

Bauxite ore processing industry in West Kalimantan generates a voluminous waste that posses potential environmental risks due to its high pH and mineral contents. However, the substantial presence of calcium, silica, aluminum, and iron in the bauxite ore processing waste (BOPW) also presents opportunities for beneficial utilization. This study investigates the potential use of BOPW as liner material in municipal solid waste landfills, in order to minimize groundwater contamination risk. Physical, chemical, mineralogical, and environmental characteristics, which comprise water content, specific gravity, particle size, toxicity characteristic leaching procedure (TCLP), atterberg limit, compaction, consolidation were measured using relevant ASTM and USEPA methods. The results showed that the BOPW exhibited favorable properties as landfill liner. The low moisture content (20.35%), cohesiveness, and specific gravity of 2.94, low hydraulic conductivity (7.56×10^{-7} cm/s) suggested suitability of the BOPW for landfill liner. Chemical analysis revealed predominant components of Fe₂O₂, Al₂O₂, SiO₂, and Na₂O₂ while mineralogical examination identified the presence of quartz, magnetite, hematite, and lime. The high pH value (11.93) supported chemical stability and immobilization of heavy metal contaminants. Despite favorable results of TCLP test, leachate quality analysis revealed elevated sodium concentrations (266 mg/L), which raised concerns about potential impact on surface water quality, particularly with the absence of specific regulatory standards. This study highlights BOPW's potential as a suitable landfill liner material, although further assessment for its long-term performance and application suitability is needed.

Keywords: bauxite processing waste, characteristics, landfill liner.

INTRODUCTION

West Kalimantan has the largest bauxite mine in Indonesia, accounting for 66.77%, or 840 million tons of the total national reserve. The Tayan subdistrict in Sanggau Regency is one of the locations with the largest bauxite reserve (Ministry of EMR, 2016). Aluminum is produced using bauxite ore as the primary raw material. The refining process of bauxite ore into alumina involves the Bayer method (Al-Sakkari et al., 2022; Mukiza et al., 2019; Salim et al., 2023), sintering (Agrawal and Dhawan, 2021; Amer, 2013), and a combination of both processes (Dubovikov and Jaskelainen, 2016).

Bauxite ore processing industry generates a fine, reddish-brown sludge residue (Manfroi et al., 2014; Shin et al., 2014). This sludge, locally named red mud, is termed as BOPW in this article. The high Fe_2O_3 content causes the BOPW to have reddish color (Carneiro et al., 2018; IAI, 2015; Lingxiang et al., 2021; Lyu et al., 2021). The various bauxite sources influence the chemical composition of the BOPW, particularly in

the levels of Al_2O_3 , SiO_2 , Fe_2O_3 , TiO_2 , and Na_2O (Nikbin et al., 2018). The Bayer process dominates the global alumina extraction method, accounting for approximately 90% of production (Gertsen, 2024; Lu et al., 2017; Tabereaux and Peterson, 2014). BOPW from the Bayer process has a higher iron content than that of sintering (Liu et al., 2014). Global annual generation of BOPW is estimated at 120 million tons (Power et al., 2011). About 1.5 to 1.6 tons of BOPW was generated as a byproduct for every ton of alumina production (Kaya and Soyer-Uzun, 2016).

BOPW exhibits high alkalinity, typically ranging from pH 10.5 to 12.5 (Shi et al., 2020; Wang et al., 2021; Wang et al., 2018). This is caused by the use of large amounts of caustic soda during the Bayer process (Shin et al., 2014). The high alkaline property makes the BOPW be classified as hazardous waste of corrosive category (Archambo and Kawatra, 2021; Zhang et al., 2018; Zhang et al., 2021). The high sodium and alkalinity contents in BOPW can potentially cause adverse environmental impacts to the environment (Díaz et al., 2015; Nikbin et al., 2018) and ecosystem damage if directly exposed (Stenchly et al., 2017; Winkler, 2014). It was also reported that the essential nature of BOPW could inhibit plant growth (Samal, 2021).

Environmental concerns which relate to improper bauxite mining waste handling has emerged recently in West Kalimantan. Public complaints arose from communities residing near bauxite mining operations. The BOPW was linked to the damage to tengkawang (Shorea stenoptera) and durian (Durio kutajensis) plantations in Melinau Regency (Anonymous, 2024) In a more recent incident, residents of Simpang Hilir Regency raised concerns about the water pollution of the Empawang River, a vital water source used by the community for bathing, sanitation, and washing. Additionally, local fishermen have reported the decline and death of fish population in this river (Anonymous, 2023). These cases highlight the potential environmental damage by the BOPW, as demonstrated by incidents worldwide. A leak at a BOPW storage facility in Hungary contaminated 1.000 hectares of land in 2010 (Gruiz et al., 2012; Mayes et al., 2011). In 2018 floods at a BOPW storage facility in Brazil caused soil contamination, which polluted water supplies with high levels of lead and aluminum (Alves, 2018). The BOPW has generally been disposed of in stockpiles (Balomenos et al., 2018). Managing BOPW in stockpiles requires approximately 2% of the cost of alumina production (Wang et al., 2019). However, the BOPW has the potentials to be used as a source of iron for steel industry (Maihatchi et al., 2020), as raw material for cement and concrete production (Hou et al., 2021; Viyasun et al., 2021), for land reclamation in heavy metal-polluted areas (Hua et al., 2017; Lockwood et al., 2014; Zhou et al., 2017), as an adsorbent for heavy metal ions (Chen et al., 2019; Du et al., 2019; López-García et al., 2017; Pepper et al., 2018), and as a liner for acid mine drainage (Duchesne and Doye, 2005).

Indonesia faces a big challenge in municipal solid waste (MSW) management, with open dumping as the predominant method. Approximately 60% of landfills in Indonesia were still operated using the this method in 2021 (KLHK, 2021). Many landfills operation with this system was due to difficulties in obtaining cover soil (Kurniasari et al., 2014). Open dump landfill operation can cause soil and groundwater contamination (IEPA, 2024; Zhang et al., 2023). The environmental impact of landfills can be mitigated by implementing appropriate barrier layers, known as liners (Nath et al., 2023; Wan et al., 2023). Typical landfill liners include clay, geosynthetic clay liners (GCL), and composite layers. The later comprises compacted clay liners (CCL) and GCL (Emmanuel et al., 2020; Shu et al., 2019). The use of clay and artificial liners has several drawbacks, which particularly related to economics consideration and availability. Clay, a valuable resource with limited availability in Indonesia, has become a big challenge in landfill construction and operation despite its varying costs. Application of clay liners shows the widest cost range (US\$32.000-162.000 per hectare). In contrast, synthetic alternatives like geomembranes (US\$24.000-35.000 per hectare) and geocomposites (US\$33.000-44.000 per hectare) offer narrower cost ranges. The integration of these liner systems substantially increases the total landfill construction costs to US\$300.000-800.000 per hectare, depending on the combination of technologies employed. The significant cost variations in landfill cover construction necessitate careful material selection and design strategies to balance environmental sustainability with economic feasibility (Rubinos and Spagnoli, 2018). Therefore, a liner made from mine waste, including the BOPW, is an alternative substitute to clay (Rubinos et al., 2015). One of landfill liner requirements is having (K) of less than 1×10^{-7} cm/s (USEPA, 1992b). Low K value can be achieved when sufficient fine particles fill the soil pores, and the absence of large particles hinders the process of compacting the soil into a dense mass (Benson and Othman, 1993).

Global industrial utilization of aluminium process waste remains limited, estimated at approximately 3% of annual generation (Evans, 2016). In Indonesia, large amounts of BOPW have not been used and are mostly haphazardly dumped. Therefore, BOPW quantity minimization is essential (Archambo & Kawatra, 2021). The BOPW can potentially be used as a primary MSW landfill liner material due to its fine particle size (average particle size $< 10 \ \mu m$) (Rubinos and Barral, 2013) and high content of Si and Al (Maritsa et al., 2016). While previous studies investigated the potential of stored BOPW aslandfill liner material (Fan et al., 2023; Kara et al., 2017; Rubinos and Spagnoli, 2018), this research was focused on the use of fresh BOPW from the Bayer process. Stored and fresh BOPW were reported to have different physical-chemical characteristics (Liu et al., 2007). Fresh BOPW, with its distinct chemical composition compared to stored BOPW, such as higher sodium content, may offer advantages in mitigating shrinkage issues commonly associated with BOPW layers. For this reason, this study, which aims to explore the characteristics and potential use of BOPW from West Kalimantan for landfill liner material, as a novel investigation.

At least there are 4 adjacent regencies to the bauxite mining in Tayan district, which urgently need cover material for landfill operation. These regencies, namely Sanggau, Kubu Raya, Sekadau, and Ketapang, still use open dump MSW landfill (Figure 1) method due to the inavailability of clay cover material. The current volume of dumped BOPW in the study area is approximately 396,600 m³. For this reason, this research. Results of this research are expected to provide a solution for BOPW management in the mining industry and a new alternative substitute for landfill liner.

MATERIALS AND METHODS

Sampling locations

The BOPW samples were obtained from the Indonesia Chemical Alumina mining company, which generated about 0.6 million metric tons of BOPW annually in Tayan Hilir District. The sampling site was located at coordinates 0°03'40.9"S and 110°08'38.4"E (Figure 2).

Sample collection and preparation

About 150 kg fresh BOPW samples were collected using a shovel. The samples were homogenized using the shovel prior to analysis. Subsequently, the BOPW was dried in an oven at 110 °C for 24 hours and then crushed. The resulting samples were sieved using a 200-mesh screen



Figure 1. Locations of BOPW stockpile, MSW landfills, and the adjacent regencies requiring landfill liner



Figure 2. Sampling location

for thermogravimetric analysis (TGA), X-ray diffraction (XRD), and toxicity characteristic leaching procedure (TCLP) analyses. The samples that passed through a 325-mesh screen was specifically used for XRD analysis.

Characterization of materials

Physical properties

The water content of the BOPW samples was determined according to ASTM D 2216-10, a standard test method for laboratory determination of water content of soil and rock. The moisture content was calculated using Equation 1.

$$Water content =$$

$$= \frac{Weight of evaporated water}{Weight of dry sample} \times 100\%^{(1)}$$

Determination of soil specific gravity (Gs) was conducted following the standard test method for specific gravity of soil solids using a water pycnometer (ASTM D854-58). The specific gravity was calculated using Equation 2.

$$G_S = \frac{W_4}{(W_3 + W_4) - W_2} \tag{2}$$

where: W_1 is weight of pycnometer and dry BOPW, W_2 is weight of water, BOPW, and W_3 is weight of pycnometer and distilled water, and W_4 is dry weight of BOPW (W_1 – the weight of empty pycnometer).

Particle size analysis of the BOPW was performed following standard test methods for particle-size distribution of soils using sieve analysis (ASTM D6913-04) and standard test method for amount of material in soil finer than the No. 200 (75-μm) Sieve (ASTM D1140-14). Hydrometer analysis was conducted according to Standard test methods for particlesize distribution of fine-grained soils using the sedimentation analysis (ASTM D7928-16).

Chemical properties

The pH of the sample material was measured by mixing 1 g of sample with 5 mL of deionized water in a vial. The resulting mixture was agitated at 650 rpm in a shaker for 10 mins. The pH was then determined using a pH meter (Eutech pH 150). Chemical composition of the BOPW was determined using X-ray fluorescence (XRF) instrument. Mineral concentrations were expressed as % weights of Fe₂O₃, Al₂O₃, SiO₂, Na₂O, TiO₂, CaO, SO₃, K₂O, MgO, P₂O₅, MnO₂, and Cr₂O₃.

Crystal structure and mineral content

The mineralogical and crystal structure analyses of the BOPW sample were performed using XRD with K-alpha radiation ($\lambda = 1.5406$ Å). The XRD data, collected over a 2 θ range of 10° to 90°, were processed using Match software (versions 2 and 3) and the international centre for diffraction data (ICDD) database to identify mineral phases and their relative percentages.

Thermal analysis

The TGA was performed for characterizing the behavior change of the BOPW sample during heating and decomposition. The material mass was measured under controlled conditions during heating or cooling processes (Yao et al., 2022). The standard test for TGA analysis was based on ASTM E1131-20 concerning standard test method for composition analysis by thermogravimetry. Sample heating process used Mettler Toledo TGA-DSC instrumentation and Huber CC 415 for cooling. Precisely 9.0405 mg sample was used for this analysis. The sample was heated from 25 °C to 1000 °C at a constant heating rate of 10 °C / min, which was maintained under a constant oxygen flow of 100 mL/min during the test.

Toxicity test

The TCLP test which determined whether a waste material is hazardous or not was applied using EPA Method 1311 (USEPA, 1992a). The results were compared to the regulatory quality standards according to Government Regulation of the Republic of Indonesia No. 22 Year 2021 concerning Environmental Protection and Management.

Geotechnical and hydraulic properties

Geotechnical characterization of the BOPW sample was conducted to assess its suitability as liner material. It included Atterberg limit tests comprising liquid limit (LL), plastic limit (PL), and (PI), compaction, and consolidation tests. Atterberg limits were determined according to ASTM D4318-17. Compaction tests were performed according to the Proctor method as specified by ASTM D698, while consolidation tests followed ASTM D2435. Consolidation data were used to establish the void ratio-log pressure relationship and calculate consolidation parameters. Consolidation parameters, including compression coefficient (Cc), (Cs), and coefficient of consolidation (Cv), were determined using the approach outlined in Equation 3-4.

$$Cc = \frac{\Delta e}{Log^{\sigma_2}/\sigma_1} \tag{3}$$

$$Cs = \frac{\Delta e}{\log^{\sigma_1}/\sigma_2} \tag{4}$$

$$Cv = \frac{0.848 \, H^2}{t_{90}} \tag{5}$$

where: Δe represented the change in void ratio between initial and final states, and σ denoted the applied pressure in kg/cm².

The swelling index was determined from the unloading portion of the consolidation test data. The time to achieve 90% consolidation (t_{90}) was obtained from the Taylor's time-fitting method

applied to the consolidation curve, where H represented half the initial sample height.

Following proctor compaction, the hydraulic conductivity of the compacted BOPW was measured at the optimum moisture content using a rigid-wall falling-head permeameter. Distilled water was used as the permeant fluid. The hydraulic conductivity value was calculated using Equation 6 presented by Das et al. (1995).

$$K = \frac{aL\ln(h_1/h_2)}{At} \tag{6}$$

where: *a* represented the cross-sectional area of the vertical pipe (cm²), *L* denoted the specimen height (cm), and *A* denoted the cross-sectional area of the BOPW (cm²). h_1 indicated the initial head (cm), h_2 represented the head at time *t* (s), and *k* represented the hydraulic conductivity (cm/s).

RESULTS AND DISCUSSION

Physical properties

Moisture

The average moisture content of the BOPW material was 20.35% (Table 1). This value was lower than the previously reported ranges of 28% to 35.21% (Chen et al., 2023; Deelwal et al., 2014; Panda et al., 2017; Salih et al., 2020). This was likely due to the dewatering stage of the fresh BOPW prior to disposal. The process, which generally used a filter press equipment, could effectively reduced the moisture content in the BOPW to less than 35% (Hanumantha and Reddy, 2017)

Liner materials, even within the same classification, often exhibited significant variability in their initial moisture content, a factor which can profoundly impact their in-situ performance. Initial water content varied for each soil type. Clay soils generally exhibited moisture levels between 22.7% and 32.3% (Hamdi and Srasra, 2013; Wang et al., 2024). Silt soils fall within a range of 14% to 22.49% (Cheng et al., 2022; Du et al., 2023; Ma et al., 2023). In contrast to other materials, bentonite had a wider water content range, between 10.6% and 40% (El-Shamy et al., 2015; Muhmed et al., 2022; Zhang et al., 2022). Conversely, residual soil had a range of water content between 20.68 to 48.08% (Wibawa et al., 2018).

Water content affected the effectiveness of materials in the field of geotechnical engineering,

especially during the use of liners (Rowe, 2005). High water content can had a negative impact on liner performance. This was because water filled the pore space, which causes effective stress between soil particles, thereby increasing the permeability value of the material (Li et al., 2022). Additionally, fluctuations in water content caused significant volume changes that have an impacted on cracking and reduced the service life of the liner (Surbakti, 2021; Wulandari and Tjandra, 2019).

The low water content of the BOPW indicated its potential as a promising liner material. The water content of the BOPW was lower when compared to conventional liners that were commonly used. This allowed the BOPW to have a permeability value that was not much different from conventional liners. In addition, the BOPW also had the potential to have resistance to volume changes that can cause cracks. Variations in different water content values affected the physical and mechanical properties of materials such as shear strength, density and ability to absorb water. All three were properties that affected the effectiveness and long-term durability of the liner material. However, material with a high water content did not mean that it could not be used as a liner, this material can still be used if it went through a series of processing steps such as drying (Du et al., 2024; John et al., 2023; Salih et al., 2020).

Particle size

The results of the hydrometer analysis and particle size distribution test showed that the BOPW consisted of 29.98% clay, 52.13% silt and 17.89% sand (Figure 3). Not less than 82.11% of the material passed the 200 mesh (0.075 mm) sieve, which was consistent with the research conducted by Chen et al., 2023 who reported a 55% pass rate of BOPW. Figure 4 (a-f) illustrates the BOPW particles retained on sieves #10, #20, #40, #100 and #200 and the fraction passing sieve #200. Permeability is the ability of a material to drain water. The permeability value is significantly influenced by the grain size of the material (Marschalko et al., 2021). The size of the material particles is directly proportional to their permeability value. This is because, when the particle size decreases, the pore space of the material shrinks and the flow path becomes more tortuous, resulting in decreased permeability (Lu et al., 2024; Marschalko et al., 2021; Zhang et al., 2020). The BOPW, dominated by clay and silt, indicates a low permeability value. This showed that the BOPW can be used for geotechnical applications.

The BOPW sample fell into the silty clay loam category according to the USDA soil texture classification system. This fine-grained soil typically exhibited cohesive properties (Hanumantha and Reddy, 2017; Kumar et al., 2023; Panda et al., 2017). The BOPW composition, characterized by a high proportion of both silt and clay, was expected to exhibit a fine texture, moderate water retention capacity, and a potential for drainage contingent upon the precise silt-clay ratio (Montelli et al., 2017; Zhang et al., 2021).

Despite its fine-grained texture, the BOPW exhibited a specific gravity of 2.77, which was notably higher than typically observed in clay



Figure 3. Distribution of particle sizes in BOPW

Parameter	Value (%)					
Gs	2.77					
Water content	20.35					
Maximum water content-(Wc)	21.9					
Size range (mm)						
0.001–0.0040	29.98					
0.0041–0.075	52.13					
0.076–2.0	17.89					
2.1–4.76	0					

Table 1. Physical Properties of BOPW

soils. This value fell within the range of 2.7–3.45, as reported for similar materials (Chen et al., 2023; Kumar et al., 2023; Li et al., 2023). The presence of Fe oxides, particularly hematite and magnetite, within the BOPW matrix was likely responsible for this elevated specific gravity, as suggested by previous researchers (Hanumantha and Reddy, 2017; Salih et al., 2020).

Chemical properties

pH value

The measured pH of BOPW was 11.93, consistent with previous reports indicated a pH range of 11–12 for similar materials (Khaerunisa et al., 2015; Santi, 2018). This value was significantly higher than typical pH ranges observed in various soil types. Clay soils typically exhibited pH values between 4.5 and 7.5 (Bessaim et al., 2018; Momeni et al., 2022), while silt soils tended to have a neutral to slightly acidic pH, generally ranging from 6 to 7 (Al-Jabban et al., 2017). Residual soils demonstrated a wider range of pH values, influenced by the parent material and mineral composition (Foss and Segovia, 2020; Simon et al., 2021).

The pH value of a material could significantly influence its surface chemistry and, consequently, its interaction with polar molecules such as water. Materials that exhibited high pH values typically possessed a strong cation exchange capacity, suggesting that the BOPW, with its high pH, could potentially function as an adsorbent (Gray et al., 2016). The pH level significantly impacted the adsorption process. At low pH, the abundance of H₂O⁺ ions lead to competition between these ions and heavy metal cations for adsorption sites on the negatively charged surface. Conversely, under high pH conditions, the reduced concentration of H₂O⁺ ions facilitated the predominance of heavy metal ions in the adsorption process, primarily driven by electrostatic interactions (Al-Jabban et al., 2017). It is important to note that acidic soil pH can lead to increased soil permeability (Momeni et al., 2022), which may have implications for the material's performance as a liner or adsorbent.



Figure 4. Photomicrographs of BOPW: (a) retained on sieve 10 mesh, (b) retained on sieve 20 mesh, (c) retained on sieve 40 mesh, (d) retained on sieve 100 mesh, (e) retained on sieve 200 mesh, (f) passed through a 200 mesh sieve, at 50 x magnifications

Chemical composition

Results of XRF analysis revealed that the chemical composition of the primary component in BOPW dominated by Al_2O_3 , SiO_2 , Fe_2O_3 , and Na_2O (Table 2). Microscopic imaging at 50x magnification showed white grains, indicative of excess sodium, while black grains were identified as metallic iron (Figure 4). The dominant reddish color of the BOPW indicated a high iron content. The chemical composition of the studied BOPW aligned with that reported for BOPW in China (Du et al., 2019; Hu et al., 2019; Lima et al., 2017). The high Na_2O content, a basic oxide, in the BOPW studied suggested a higher pH value compared to clay (Zhang et al., 2018).

The BOPW composition shared similarities with mineral composition of clay, which was typically dominated by SiO_2 (46.40–85.51%) and Al_2O_3 (2.96–39.63%) (Onyelowe et al., 2023; Purbasari and Samadhi, 2021) and Al_2O_3 (2.96–39.63%) (Dewi et al., 2018, 2020). In contrast, residual soil was generally dominated by iron with a range of 52–75% (Silva et al., 2018); whereas Na-bentonite clay tended to have a higher silica content compared to its aluminum content (Kumar and Lingfa, 2020).

Crystal structure and mineral content

Results of XRD analysis showed quartz, magnetite, hematite, and lime as the primary mineral

10

20

30

0

constituents of the investigated BOPW (Figure 5). Notably, gibbsite and boehmite, commonly found in other BOPW sources, were absent, indicating a distinct mineralogical composition (Li et al., 2023; Ramdhani et al., 2023; Wu and Liu, 2012). The high iron contents in BOPW were found in the form of hematite (Fe₂O₃) and magnetite (Fe₃O₄) (Liu et al., 2023; Sun et al., 2019). The high presence of silica was originated from its removal from bauxite ore during the Bayer process (Tabereaux and Peterson, 2014). Wu and Liu (2012) suggested that materials containing quartz could be used as adsorbents.

Thermal stability and decomposition

The TGA analysis showed that exothermic process occured at temperatures > 700 °C over a period ranging from 69 to 96 min, peaking at 716 °C (Figure 6). Pre-dehydroxylation and hydroxylation processes occured during the endothermic phase (Saukani et al., 2020; Waluyo et al., 2022). The endothermic process occured at temperatures < 700 °C over a period ranging from 0 to 68 min, peaking at 265 °C. This process took place within the temperature range of 300–700 °C. Organic materials underwent decomposition within the 200–600 °C temperature range (Wang et al., 2020). The percentage of material mass lost during combustion up to 1000 °C is 15.2%, which indicated that inorganic compounds dominate the

Motorial	Parameters (% wt)												
Material	Al ₂ O ₃	SiO ₂	Fe ₂ O ₃	CaO	Na ₂ O	TiO ₂	MgO	K ₂ O	SO3	P ₂ O ₅	MnO ₂	Cr ₂ O ₃	LOI
BOPW	18.9	18.78	29.81	1.45	17.89	1.76	0.14	0.14	0.42	0.13	0.06	0.05	10.23



Figure 5. XRD analysis result of the BOPW

50 2θ (⁰) 60

70

80

90

40

Table 2. Chemical composition of BOPW



Figure 6. The TGA analysis curve of BOPW

BOPW material. Inorganic materials generally exhibit high surface area criteria, small pore sizes, and good hydrothermal stability, which made them a favorable choice for effective adsorption processes (Yeom and Kim, 2017; Zhang et al., 2015). Additionally, materials with high adsorption capacity were suitable for use as liners as they can reduce fluid movement and adsorb pollutants (Lakshmikantha and Sivapullaiah, 2006).

Toxicity

Results of TCLP analysis of the BOPW material revealed that concentrations of inorganic parameters and anions were below Indonesian regulatory standards (Table 3). As iron is not specifically included in Indonesia's TCLP criteria, a conservative assessment was employed. This involved the use of drinking water quality standards for iron by multiplying a 100-fold safety factor as suggested by Intrakamhaeng et al. (2020). The results confirmed that heavy metal iron content was significantly lower than this limit.

Geotechnical and hydraulic properties

The Atterberg limit test results revealed that the BOPW has a liquid limit of 29.25%, a plastic limit of 22.09%, and a plasticity index of 7.16% (Table 4). Based on these values, the unified soil classification system (USCS) categorizes the BOPW as clay mineral (inorganic silt) with

Parameter	Test result (mg/L)	Quallity standards (mg/L)		
Arsenic	< 0.003	0.5 **		
Barium	0.21	35 **		
Boron	< 0.10	25 **		
Cadmium	< 0.06	0.15 **		
Copper	< 0.06	10 **		
Total Cyanide	< 0.03	3.5 **		
Fluoride	1.8	75 **		
Lead	< 0.07	0.5 **		
Mercury	< 0.0003	0.05 **		
Nitrate	4.0	2.500 **		
Nitrite	< 0.03	150 **		
Selenium	< 0.0003	0.5 **		
Silver	< 0.10	5 **		
Zinc	0.13	50 **		
Antimony	< 0.10	1 **		
Berilium	< 0.0027	0.5 **		
Molibdenum	< 0.037	3.5 **		
Nickel	< 0.10	3.5 **		
Chromium hexavalent	0.33	2.5 **		
Chloride	20.8	12.500 **		
Iron	0.29	20 *		
lodide	< 0.04	5 **		

Note: *Indonesian Regulatory Drinking Water Quality Standards, Ministry of Health Regulation No.2 Years 2023 (This parameter is multiplied by 100), **Regulatory Standards for Toxicity Characteristics through the TCLP in Indonesia, Government Regulation No. 22 Years 2021.

Parameter	Result	Unit
LL	29.25	%
PL	22.09	%
PI	7.16	%
SL	2.70	%
γd	1.68	g/cm ³
n	0.39	
е	0.64	
К	7.56 x10 ⁻⁷	cm/s

Table 4. Geotechnical and hydraulic properties

low plasticity. This classification aligns with previous research conducted in Spain (Rubinos et al., 2015). The calculated LL and PI values of BOPW exceed the minimum requirements (LL > 20 and PI > 7) to achieve a hydraulic conductivity of 1×10⁻⁷ cm/s (Benson and Othman, 1993; Daniel, 1993). While materials with PI > 30-40%generally exhibited higher shrinkage potential, and the BOPW with significantly lower PI value than 7%, indicated a lower shrinkage potential (Daniel, 1993). An activity ratio (PI/clay fraction) of 0.24, suggests that the BOPW can be classified as an inactive clay. This implied that the BOPW had a low tendency to swell or shrink (Skempton, 1953). Despite its low activity, the BOPW still had potential for use as a liner, provided it had a hydraulic conductivity value less than 1×10^{-7} cm/s. (Rubinos and Spagnoli, 2018; Wang et al., 2020).

The linear shrinkage of the BOPW was 2.7%. This value fell within the criteria range of BOPW from bauxite refineries of 1.5% to 4.2% (Rubinos et al., 2015; Wang and Liu, 2012). Shrinkage and plasticity were directly related properties influenced by factors such as particle size distribution, mineralogical composition (including mineral type and crystallinity), and the type of exchangeable cations present. The relatively low shrinkage value of the BOPW was attributed to the high sodium content, as sodium was known to mitigate shrinkage by reducing the material's sensitivity to moisture changes (Rubinos and Spagnoli, 2018). This low shrinkage potential was beneficial as it reduced the likelihood of cracking within the material.

Standard proctor compaction testing of the BOPW yielded a characteristic curve mirrored the behavior of clayey soils, where dry density increased with moisture content to a maximum value, followed by a decrease with further water (Chaiyasat, 2019). A maximum dry unit weight (γ d) of 1.68 g/cm³ was achieved at an optimum water content (Wc) of 21.9%. Compacting the raw material at its optimum moisture content produced a highly homogeneous and dense material. Analysis at the maximum dry weight revealed a porosity (n) of 0.391 and an associated void ratio (e) of 0.64. These parameters were found to exert an indirect influence to better infiltration characteristics of the material.

The measured BOPW hydraulic conductivity (K) was low 7.56×10^{-7} cm/s, which met the USEPA standards for liner applications of 1×10^{-7} cm/s. The low hydraulic conductivity is influenced by the inherent properties and particle size distribution of the soil. However, the base layer of landfills might deform shear due to the MSW weight burden, which potentially caused cracks in the liner. The load had the potential to damage the underlying protective layer, allowing leachate from the MSW heap to contaminate groundwater. The deformability of the landfill liner under MSW load was primarily governed by its compressibility.

Consistency tests of the BOPW resulted in a compression coefficient (Cc) of 0.078, a swelling coefficient (Cs) of 0.033, an initial void ratio (e) of 0.64, and a coefficient of consolidation (Cv) of 2.27×10^{-6} m²/s. The Cc value suggested moderate compressibility, implied that the liner will underwent a moderate degree of settlement under waste loading. This settlement can potentially enhance the liner's density, further reduced its permeability over time. However, it was crucial to ensure that the settlement did not induce cracking or discontinuities within the liner, which could compromised its integrity.

The low swelling coefficient of 0.033 indicates minimum expansion potential of the material when subjected to unloading or wetting. This characteristic was advantageous in coating material applications as it minimized the risk of cracking or significant volume changes due to moisture fluctuations or loading. The average consolidation coefficient (Cv) of 2.27×10^{-6} m²/s suggested a relatively slow consolidation rate. This slow consolidation rate was beneficial in landfill applications as it allows gradual adjustment to loads without the sudden cracking, although it may require longer construction times to achieve optimal compaction. The initial void ratio of 0.64, which decreased with increasing

No	σ (consolidation pressure) (kg/cm ²)	Cv (10 ⁻³ cm²/s)	е	Mv (coefficient of volume compressibility) (cm²/kg)	K (10 ⁻⁷ cm/s)	Cv _{pairwaise average} (10 ⁻³ cm ² /s)	K _{average} (10 ⁻⁷ cm/s)
1	0.250	0.841	0.510				
2	0.500	3.424	0.459	0.125	2.610	2.132	
3	1.000	3.502	0.403	0.067	1.502	3.463	0.607
4	2.000	1.477	0.370	0.019	4.452	2.490	2.007
5	4.000	2.496	0.347	0.007	1.600	1.986	
6	8.000	1.896	0.251	0.015	3.270	2.196	

Table 5. Post-consolidation hydraulic conductivity values

load, indicated the potential for further compaction of the material under waste loads. This progressive compaction can enhanced the long-term effectiveness of the liner in preventing leachate seepage. The post-consolidation hydraulic conductivity of the material at each loading stage was determined based on the consolidation coefficient and volume compressibility coefficient obtained from consolidation testing. Analysis results indicated an average hydraulic conductivity of 2.687×10^{-7} cm/s (Table 5).

This low permeability is a highly desirable characteristic for landfill liner application, which met the typical regulatory requirement of less than 1×10^{-7} cm/s. Such low permeability effectively minimized leachate infiltration into the underlying soil, thus protecting groundwater resources from contamination. The consistency of hydraulic conductivity test results between the falling head method and consolidation test strengthened the validity of this study's findings.

Despite the low hydraulic conductivity of the BOPW, leachate analysis revealed the release of sodium and iron, reaching concentrations of 266 mg/L and 0.27 mg/L, respectively. Although the iron concentration did not yet reached the safe threshold for drinking water (0.3 mg/L according to Indonesian standards), the elevated sodium concentration in the leachate, reaching 266 mg/L, necessitates further investigation, eventhough specific regulatory standards for sodium in surface water have yet to be established. High sodium content can inhibit the performance of the leachate processing unit, so further research is needed. In addition to its potential as a landfill cover material, the BOPW is also able to absorb several heavy metals and dyes (Zhang et al., 2022). However, the effectiveness of its absorption is still unknown, so further research is needed. Apart from that, economic feasibility also needs to be considered in the future.

CONCLUSIONS

BOPW demonstrates significant potential as an alternative material for landfill liner. Based on its geotechnical and physicochemical characteristics, BOPW exhibits a hydraulic conductivity value that meets the requirements for use as a landfill liner. This finding provides opportunities for the mining industry to implement circular economy and clean industry principles by integrating BOPW into waste management infrastructure. Although this research yields promising results, the high sodium content requires attention. Given the significant sodium release observed in leachate analysis, and the lack of existing quality standards, comprehensive further research is crucial. Further research should investigate three key aspects: namely the potential impact of sodium release on wastewater treatment plant performance and the long-term performance of the BOPW liner. In addition, research on its economic feasibility analysis is also needed. Despite facing challenges, the potential of BOPW as a substitute for clay liners remains promising. Its utilization supports the principles of clean industry by reducing reliance on natural clay and mitigating environmental impact.

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